

**UNITED STATES PATENT APPLICATION FOR:**

**FILTERED ACTUATOR PORT FOR HYDRAULICALLY ACTUATED DOWNHOLE  
TOOLS**

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## **FILTERED ACTUATOR PORT FOR HYDRAULICALLY ACTUATED DOWNHOLE TOOLS**

### **CROSS-REFERENCE TO RELATED APPLICATIONS**

[0001] This application is a continuation-in-part of co-pending U.S. patent application serial no. 10/073,685, filed February 11, 2002, which is a continuation-in-part of U.S. patent application serial no. 09/858,153, filed May 15, 2001, now abandoned, which is a divisional of U.S. patent application serial no. 09/435,388, filed November 6, 1999, which is now U.S. Patent No. 6,253,856, issued July 3, 2001. All of which are herein incorporated by reference in their entireties.

### **BACKGROUND OF THE INVENTION**

#### **Field of the Invention**

[0002] This invention is related to downhole tools for a hydrocarbon wellbore. More particularly, the invention relates to an apparatus useful in conducting a fracturing or other wellbore treating operation. More particularly still, this invention relates to a filtered inlet port through which a wellbore treating fluid such as a "frac" fluid may be pumped without obstructing the workings of a hydraulic tool.

#### **Description of the Related Art**

[0003] In the drilling of oil and gas wells, a wellbore is formed using a drill bit that is urged downwardly at a lower end of a drill string. When the well is drilled to a first designated depth, a first string of casing is run into the wellbore. The first string of casing is hung from the surface, and then cement is circulated into the annulus behind the casing. Typically, the well is drilled to a second designated depth after the first string of casing is set in the wellbore. A second string of casing, or liner, is run into the wellbore to the second designated depth. This process may be repeated with additional liner strings until the well has been drilled to total depth. In this manner, wells are typically formed with two or more strings of casing having an ever-decreasing diameter.

[0004] After a well has been drilled, it is desirable to provide a flow path for hydrocarbons from the surrounding formation into the newly formed wellbore. Therefore, after all casing has been set, perforations are shot through the liner string at a depth which equates to the anticipated depth of hydrocarbons. Alternatively, a liner having pre-formed slots may be run into the hole as casing. Alternatively still, a lower portion of the wellbore may remain uncased so that the formation and fluids residing therein remain exposed to the wellbore.

[0005] In many instances, either before or after production has begun, it is desirable to inject a treating fluid into the surrounding formation at particular depths. Such a depth is sometimes referred to as "an area of interest" in a formation. Various treating fluids are known, such as acids, polymers, and fracturing fluids.

[0006] In order to treat an area of interest, it is desirable to "straddle" the area of interest within the wellbore. This is typically done by "packing off" the wellbore above and below the area of interest. To accomplish this, a first packer having a packing element is set above the area of interest, and a second packer also having a packing element is set below the area of interest. Treating fluids can then be injected under pressure into the formation between the two set packers.

[0007] A variety of pack-off tools are available which include two selectively-settable and spaced-apart packing elements. Several such prior art tools use a piston or pistons movable in response to hydraulic pressure in order to actuate the setting apparatus for the packing elements. However, debris or other material can block or clog the piston apparatus, inhibiting or preventing setting of the packing elements. Such debris can also prevent the un-setting or release of the packing elements. This is particularly true during fracturing operations, or "frac jobs," which utilize sand or granular aggregate as part of the formation treatment fluid.

[0008] Prior solutions to the debris problem have included running in a filter or screen above the down-hole tool. This has several disadvantages. First, once the screen is run above the down-hole tool, full pressure can no longer be transmitted to

the piston. Second, emergency release mechanisms and other devices actuated by a ball cannot be used.

[0009] There is, therefore, a need for a hydraulic down-hole tool which does not require a piston susceptible to becoming clogged by sand or other debris.

### **SUMMARY OF THE INVENTION**

[0010] The present invention generally discloses a novel actuator port for use in a hydraulic wellbore tool, a method of making the actuator port, and methods of using the actuator port. The actuator port filters out particulates so they do not obstruct the workings of the actuator. The filtered port may comprise fine slots disposed through a wall of a mandrel spaced around the circumference of the mandrel.

[0011] The present invention introduces a hydraulic tool for use in a wellbore, comprising: a tubular wall for separating a first fluid containing region from a second fluid containing region, the tubular wall including a filter portion; and an actuating member disposed within the second fluid containing region, the actuating member operable upon contact with a fluid flowing from the first fluid containing region and through the filter portion.

[0012] The present invention discloses forming at least one filter slot in the tubular wall utilizing manufacturing methods including but not limited to electrical discharge machining and laser cutting.

[0013] The present invention may be incorporated into any kind of hydraulic tool, including but not limited to a packer comprising a packing element and a fracture valve comprising a fracture port. These may be provided into a pack-off system comprising an upper packer, a fracture valve, and a lower packer all utilizing the present invention. The pack-off system may include other components as well.

[0014] The pack-off system utilizing the present invention may be run into a wellbore where the packing elements are set and the fracture port is opened by

injecting fluid into the packer system under various flow rates resulting in various pressures. Further, an actuating fluid may be used to set the packers and open the fracture valve, and then treatment fluid may be injected through a fracture port into the wellbore.

### **BRIEF DESCRIPTION OF THE DRAWINGS**

[0015] So that the manner in which the above recited features of the present invention can be understood in detail, a more particular description of the invention, briefly summarized above, may be had by reference to embodiments, some of which are illustrated in the appended drawings. It is to be noted, however, that the appended drawings illustrate only typical embodiments of this invention and are therefore not to be considered limiting of its scope, for the invention may admit to other equally effective embodiments.

[0016] Figure 1 is a view of one cross-section of a hydraulic packer utilizing a filtered actuator according to one embodiment of the present invention. Figure 1A is a section of Figure 1 detailing a filtered inlet port. Figure 1B is a cross-sectional view of a nozzle valve.

[0017] Figure 2 is a cross-sectional view of a fracture valve utilizing a filtered actuator according to one embodiment of the present invention. Figure 2A is an enlargement of a piston / mandrel interface of Figure 2.

[0018] Figures 3A-3D are section views of a completed pack-off system. Figure 3A is the system in the run in position. Figure 3B is the system after the nozzle valve has been closed. Figure 3C is the system after the packers have been set. Figure 3D is the system after opening of the fracture valve.

### **DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT**

[0019] FIG. 1 presents a sectional view of a hydraulic packer 1 as might be used with a filtered port of the present invention. The packer is seen in a run in

configuration. The packer **1** first comprises a packing element **40**. The packing element **40** may be made of any suitable resilient material, including but not limited to any suitable elastomeric or polymeric material. Actuation of the packing element below a workstring (not shown) is accomplished, in one aspect, through the application of hydraulic pressure.

[0020] Visible at the top of the packer **1** in **FIG. 1** is a top sub **10**. The top sub **10** is a generally cylindrical body having a flow bore therethrough. The top sub **10** is threadedly connected at a top end to the workstring (not shown) or a fracture valve (as shown in **FIG. 2**). At a lower end, the top sub **10** is threadedly connected to an element adapter **20**. The element adapter **20** defines a tubular body surrounding a lower portion of the top sub **10**. An o-ring **13** seals a top sub **10** / element adapter **20** interface. At a lower end, the element adapter **20** is threadedly connected to a center mandrel **15**. The center mandrel **15** defines a tubular body having a flow bore therethrough. The lower end of the element adapter **20** surrounds an upper end of the center mandrel **15**. One or more o-rings may be used to seal the various interfaces of the packer **1**. In one embodiment, an o-ring **12** seals an element adapter **20** / center mandrel **15** interface.

[0021] The packer **1** shown in **FIG. 1** also includes a packing element compressor **30** and a piston **45**. The packing element compressor **30** and the piston **45** each generally define a cylindrical body and each surround a portion of the center mandrel **15**. An o-ring **14** seals a packing element compressor **30** / center mandrel **15** interface. An upper end of the piston **45** is disposed within and threadedly connected to the packing element compressor **20**. An o-ring **16** seals a packing element compressor **30** / piston **45** interface. Surrounding a lower end of the packing element compressor **30** and threadedly connected thereto is an upper gage ring **5**. The upper gage ring **5** defines a tubular body and also surrounds a portion of the piston **45**. At a lower end, the upper gage ring **5** comprises a retaining lip that mates with a corresponding retaining lip at an upper end of the packing element **40**. The lip of the upper gage ring **5** aids in forcing the extrusion of the

packing element **40** outwardly into contact with the surrounding casing (not shown) when the packing element **40** is set.

[0022] At a lower end, the packing element **40** comprises another retaining lip which corresponds with a retaining lip comprised on an upper end of a lower gage ring **50**. The lower gage ring **50** defines a tubular body and surrounds a portion of the piston **45**. At a lower end, the lower gage ring **50** surrounds and is threadedly connected to an upper end of a center case **55**. The center case **55** defines a tubular body which surrounds a portion of the piston **45**. Within the center case **55**, the piston **45** defines a chamber **60**. Corresponding to the chamber **60** is a filtered inlet port **65** disposed through a wall of the center mandrel **15**. Preferably, the filtered inlet port **65** comprises two sets of filter slots.

[0023] Each filter slot **65** is configured to allow fluid to flow through but to prevent the passage of particulates. Preferably, the filter slots are substantially rectangular in shape. In one embodiment shown in **FIG. 1A**, ten filter slots **65** are equally spaced around the entire circumference of the center mandrel for each set of inlet slots. The filter slots **65** can be cut into the center mandrel **15** using a laser or electrical discharge machining (EDM). The dimensions and number of slots may vary depending on the size of the particulates expected in the fracture fluid. As an example, for a fracture fluid with a minimum particulate size of 0.016 inch in diameter, each filter slot **65** would preferably be 0.9 inch long and between 0.006-0.012 inch wide. Optionally, the width of the slot **65** may be reduced down to 0.003 inch or as far as current manufacturing technology will allow. Typically, a maximum slot width of 0.02-0.03 inch would be expected, however, a width of 0.2 inch would also fall within the scope of the present invention. Use of the term "width" does not mean that the slot **65** must be rectangular. Other shapes can be used for the filter slots **65**, such as triangles, ellipses, squares, and circles. In those cases the "width" would be the smallest dimension across the slot **65** (not including the thickness of the slot through the mandrel **15**). Other manufacturing techniques may be used to form the filtered inlet port **65**, such as the formation of a powdered metal screen or

the manufacture of a sintered powdered metal sleeve with the non-flow areas of the sintered sleeve being made impervious to flow.

[0024] Disposed within the inlet slot **60** are blocks **62**. Preferably, the blocks **62** are annular plates which are threaded on both sides. The outer threads of the blocks **62** mate with threads disposed on an inner side of the center case **55**. The inner threads of the blocks **62** mate with threads disposed on an outer side of the center mandrel **15**. The blocks are disposed on the center mandrel **15** just below a lower set of filtered inlet slots **65**. Preferably, the blocks **62** further comprise a tongue disposed on an upper end for mating with a groove disposed on the outside of the central mandrel **15**. Preferably, the blocks **62** do not completely fill the inlet slot **60**, thereby leaving a gap allowing fluid to flow around the blocks within the inlet slot.

[0025] An o-ring **17** seals an upper piston **45** / center case **55** interface. An o-ring **18** seals a lower piston **45** / center case **55** interface. An o-ring **19** seals a piston **45** / center mandrel **15** interface. Abutting a lower end of the piston **45** is an upper end of a biasing member **70**. Preferably, the biasing member **70** comprises a spring. The spring **70** is disposed on the outside of the center mandrel **15**. The lower end of the spring **70** abuts an upper end of a spring adapter **75**. The spring adapter **75** defines a tubular body. At an upper end, the spring adapter **75** surrounds and is threadedly connected to a lower end of the central mandrel **15**. At a lower end, the spring adapter **75** surrounds and is threadedly connected to a bottom sub **80**. The bottom sub **80** defines a tubular body having a flow bore therethrough. An o-ring **21** seals a spring adapter **75** / center mandrel **15** interface. A lower end of the bottom sub **80** is threaded so that it may be connected to other members of the workstring such as a nozzle valve **85** (as illustrated in **FIG. 1B**), or a fracture valve (as displayed in **FIG. 2**). An o-ring **22** seals a spring adapter **75** / bottom sub **80** interface. **FIG. 1B** contains a cross sectional view of the nozzle valve **85**. The nozzle valve **85** comprises a flow bore therethrough with a tapered seat for a ball that may be dropped through the workstring.

[0026] **FIG. 2** presents a sectional view of a fracture valve **100** as might be used with a filtered port of the present invention. The fracture valve **100** is seen in a run in configuration. Visible at the top of the fracture valve **100** in **FIG. 1** is a top sub **110**. The top sub **110** is a generally cylindrical body having a flow bore therethrough. The top sub **110** is threadedly connected at a top end to the workstring (not shown) or a packer (as shown in **FIG. 1**).

[0027] At a lower end, the top sub **110** surrounds and is threadedly connected to an upper end of a mandrel **115**. The mandrel **115** defines a tubular body having a flow bore therethrough. Set screws **105** optionally prevent unthreading of the top sub **110** from the mandrel **115**. An o-ring **113** seals a top sub **110** / mandrel **115** interface. Also at the lower end, the top sub **110** is surrounded by and threadedly connected to an upper end of a sleeve **120**. The sleeve **120** defines a tubular body with a bore therethrough. Disposed between the mandrel **115** and the sleeve **120** below the top sub is an adjusting nut **122**. The adjusting nut **122** is threadedly connected to the mandrel **115**. Abutting a lower end of the adjusting nut **122** is an upper end of a biasing member **125**. Preferably, the biasing member **125** comprises a spring. Abutting a lower end of the spring **125** is a piston **130**. **FIG. 2A** is an enlarged partial view of a piston **130** / mandrel **115** interface. The piston **130** and the mandrel **115** define a chamber **135**. Corresponding to the chamber **135** is a filtered inlet port **140** disposed through a wall of the mandrel **115**. Preferably, the filtered inlet port **140** comprises one set of filter slots. Each filter slot **140** is similar to the filter slot **65** discussed above with reference to the packer **1**. Disposed in the wall of the mandrel **115** below the filter slots **140** is a fracture port **145**. An upper o-ring **114** and a middle o-ring **116** cooperate to seal a piston **130** / mandrel **115** interface above the fracture port **145**. The middle o-ring **116** and a lower o-ring **117** cooperate to seal the piston **130** / mandrel **115** interface proximate the fracture port **145**. Abutting a lower end of the piston **130** is a bottom sub **150**. The bottom sub **150** is a generally cylindrical body having a flow bore therethrough. At an upper end, the bottom sub **150** surrounds and is threadedly connected to a lower end of the mandrel **115**. Set screws **155** optionally prevent unthreading of the bottom sub **150** from the mandrel **115**. An o-ring **118** seals a bottom sub **150** / mandrel **115**

interface. Disposed below the bottom sub **150** / mandrel **115** interface in a wall of the bottom sub **150** are jet nozzles **160**. At a lower end, the bottom sub **150** is threaded so that it may be connected to the workstring or other members thereof, such as a packer (as displayed in **FIG. 1**).

[0028] Referring to **FIGS. 3A-3D**, in operation, the packer **1** and the fracture valve **100** are run into the wellbore on the workstring, such as a string of coiled tubing, as part of a pack-off system **200**. The workstring is any suitable tubular useful for running tools into a wellbore, including but not limited to jointed tubing, coiled tubing, and drill pipe. The pack-off system **200** comprises a top packer **205**, the fracture valve **100**, the bottom packer **1**, and the nozzle valve **85** or a solid nose portion (not shown). It is understood that additional tools, such as an unloader (not shown) may be used with the pack-off system **200** on the workstring. Preferably, the top packer **205** is a slightly modified version of the bottom packer **1**. The top sub and the bottom sub are exchanged enabling the top packer to be mounted upside down in the workstring. The pack-off system may also comprise a spacer pipe (not shown) between the two packers.

[0029] In **FIG. 3A**, the pack-off system **200** is positioned adjacent an area of interest, such as perforations **242** within a casing string **240**. Once the pack-off system **200** has been located at the desired depth in the wellbore, a ball is dropped from the surface into the pack-off system **200** to seal the nozzle valve as shown in **FIG. 3B**. Fluid is injected into the system at a first flow rate sufficient to set the packers **1** and **205**. Because the flow of fluid out of the bottom of the pack-off system **200** is closed off, fluid is forced to exit the system **200** through the jet nozzles **160** of the fracture valve **100**. Flow through the jet nozzles **160** will generate a back pressure within the system. Fluid, under this back pressure, also enters the piston chambers **60** and **135** through the filter slots **65** and **140** of the packers **1** and **205** and fracture valve **100** respectively. The filter slots **65** and **140** prevent any debris in the fluid from entering the piston chambers **60** and **135**. The pistons **45** and **130** are configured such that one face of the pistons within the chambers **60** and **135** is larger than the other. This will create a net force,

generated by the pressure, on the larger piston faces. This force will be opposed by the springs **70** and **125** and, in the packers **1** and **205**, the packing elements **40**. Once the pressure is sufficient to overcome the opposing forces (the spring force of the fracture valve **100** is greater than that of the packers **1** and **205**), it will force the pistons **45** of the upper **205** and lower **1** packers downward (upward for the upper packer) since the system **200** and thus the center mandrels **15**, blocks **62**, center cases **55**, and lower gage rings **50** are held in place by the workstring. This forces the packing element compressors **30** and upper gage rings **5** to move downwardly (upwardly for the upper packer). The upper gage rings **5** push down (up for the upper packer) to set the packing elements **40** of the upper and lower packers **1** and **205**. The packing elements **40** are shown set within the casing **240** in **Figure 3C**.

[0030] After sufficient pressure has been applied to the pack-off system **200** through the bores of the center mandrels **15** to set the packing elements **40**, the fluid injection rate is increased into the system **200**. From there fluid enters the annular region between the pack-off system **200** and the surrounding casing **240**. The injected fluid is held in the annular region between the packing elements **40** of the upper **205** and lower packers **1**. Fluid continues to be injected, at this higher rate, into the system **200** and through the jet nozzles **160** until a greater second pressure level is reached. This second pressure causes the piston **130** of the fracture valve **100** to move upward along the mandrel **115**. This, in turn, exposes the fracture port **145** to the annular region between the pack-off system **200** and the surrounding casing **240** as shown in **FIG. 3D**. A greater volume of fracturing fluid can then be injected into the wellbore so that formation fracturing operations can be further conducted.

[0031] If any debris should deposit on the filter slots, it may be purged when the system is reset by de-pressurization. This is due to the fact that as the pistons **45** and **130** are urged back to their run in positions, fluid will be forced from the chambers **60** and **135** of the packers **1** and **205** and fracture valve **100** back through the filtered slots **65** and **140** into the center mandrels **15** and mandrel **115** respectively.

PATENT

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[0032] The filtered inlet ports shown in **FIGS. 1-3** may be used with any hydraulically operated tool. While the foregoing is directed to embodiments of the present invention, other and further embodiments of the invention may be devised without departing from the basic scope thereof, and the scope thereof is determined by the claims that follow.